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Nidelva River bank modification report.

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Report

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Report



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FOREWORDS

The report is part of the Samfunnets plans for expansion. These plans include a filling into Nidelva to secure the slope between Upper Bakklandet – Lower Singsaker. The objective of this study is to estimate changes in flowpattern, flow velocities, flood level and possible changes in erosion risk due to the geometry modification, stated in document code 418290-RIG-NOT-002, Multiconsult.

Thanks to Ingebrigt Bævre, Orvedal Kjartan at NVE and Knut Alfredsen for providing data for this report.

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I. INTRODUCTION

1.1. Description of the task

The report is part of the Samfunnets plans for expansion. These plans include a filling into Nidelva to secure the slope between Upper Bakklandet – Lower Singsaker. The objective of this study is to estimate changes in flowpattern, flow velocities, flood level and possible changes in erosion risk due to the geometry modification, stated in document code 418290-RIG-NOT-002, Multiconsult.

For this purpose the River Analysis System [HEC-RAS](#) is used.

1.2. Description of the waterway and modification work

The river bank modification will be started from downstream Elgeseter bru and length up to 300m. The design was consulted by Multiconsult and are displayed as below:

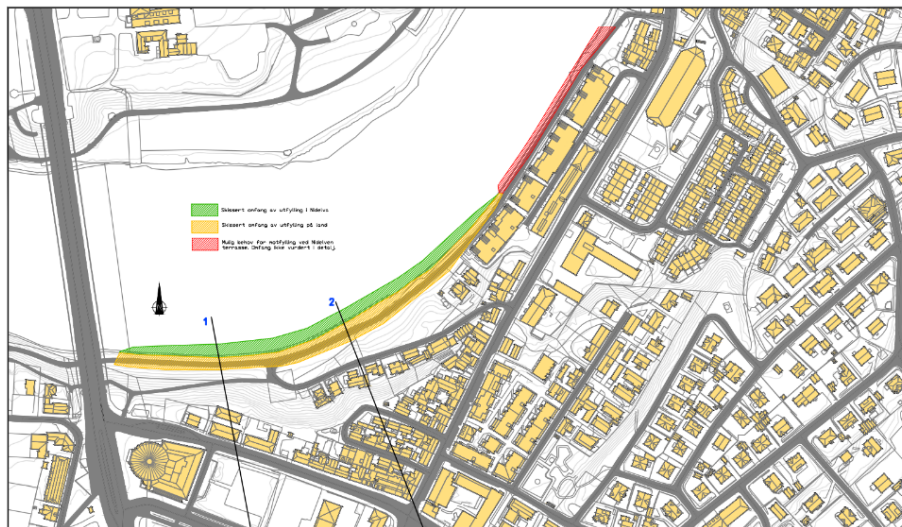


Figure 1: Riverbank design (Gylland, Feb 2017)

The filling will begin from -2.61m depth in profile 1 and -2.63m in profile 2 and extend up to 7m towards the river bed. Those parameters were used later in Hec-Ras to simulate the river flow after the modification.

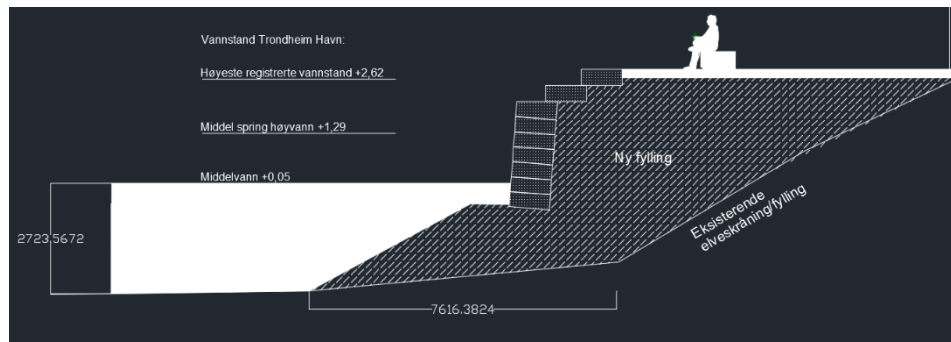


Figure 2: Cross section 1 profile

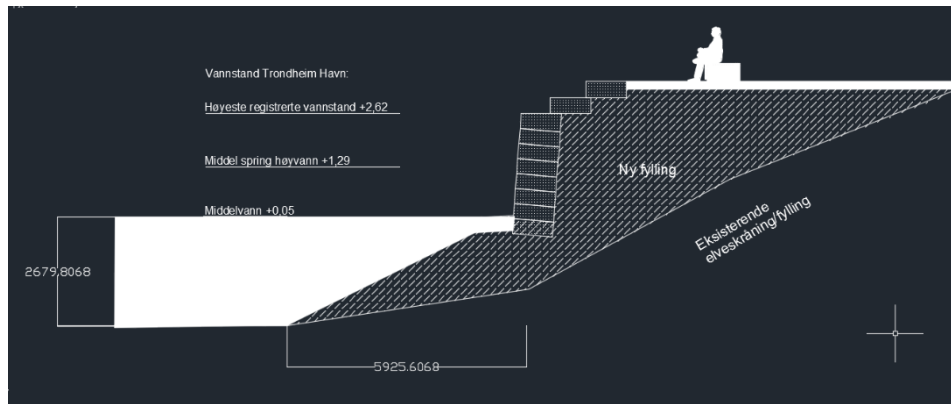


Figure 3: Cross section 2 profile

II. METHODOLOGY

HecRas was used to answer the question how river bank modification at Elgeseter Bru effects the water level and velocities. The model was built from downstream Sluppen bru to Trondheim havn, while the area of interest is from upstream Elgseter bru to about 300m downstream Elgeseter bru, or from cross section 25 → 28 in fig 4.



Figure 4: Hec-Ras model setup location

The model's geometry was built from Digital Elevation Map (DEM 1m laser dataset), downloaded from Hoydedata.no. River Cross sections profiles and flow data was provided by NVE and NTNU in various measurement campaigns. The model was calibrated using observed flood data to simulate the river flow before filling work.

After that, the geometry was adjusted to simulate the impact of the modification. 3 cross sections' parameters were changed to adapt to new geometry profile and are displayed as below:

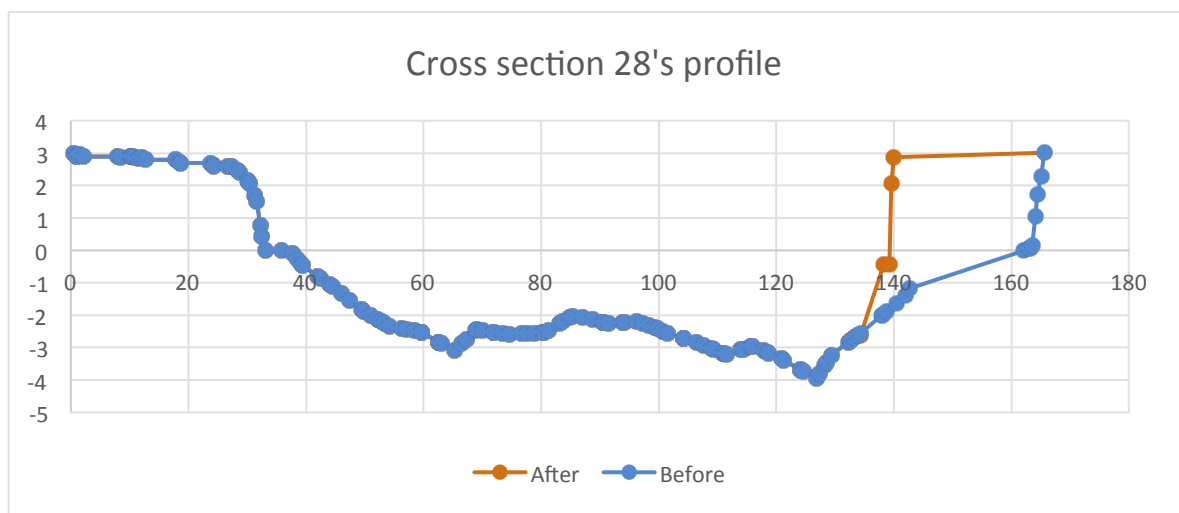
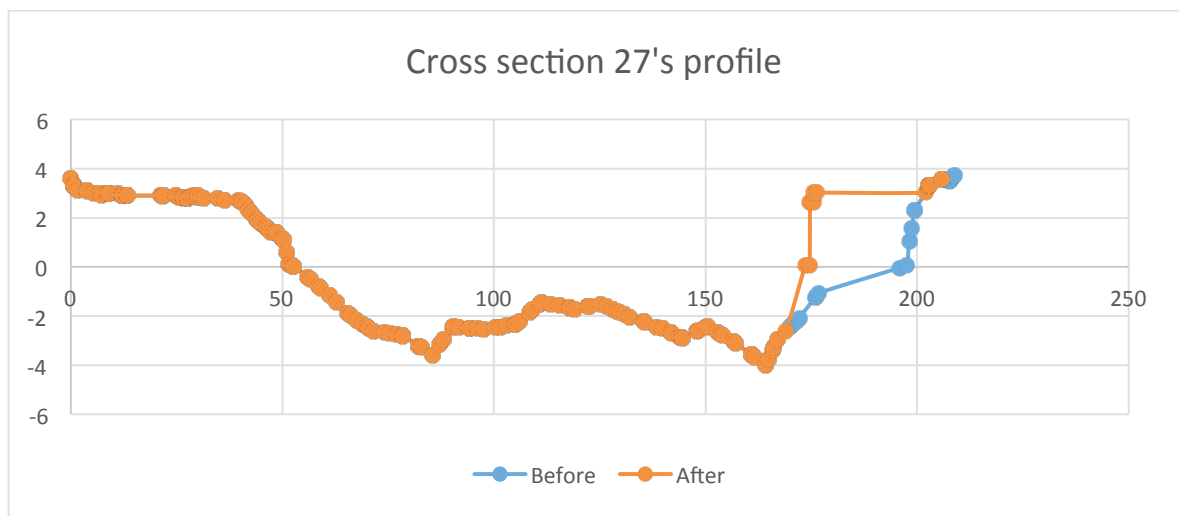
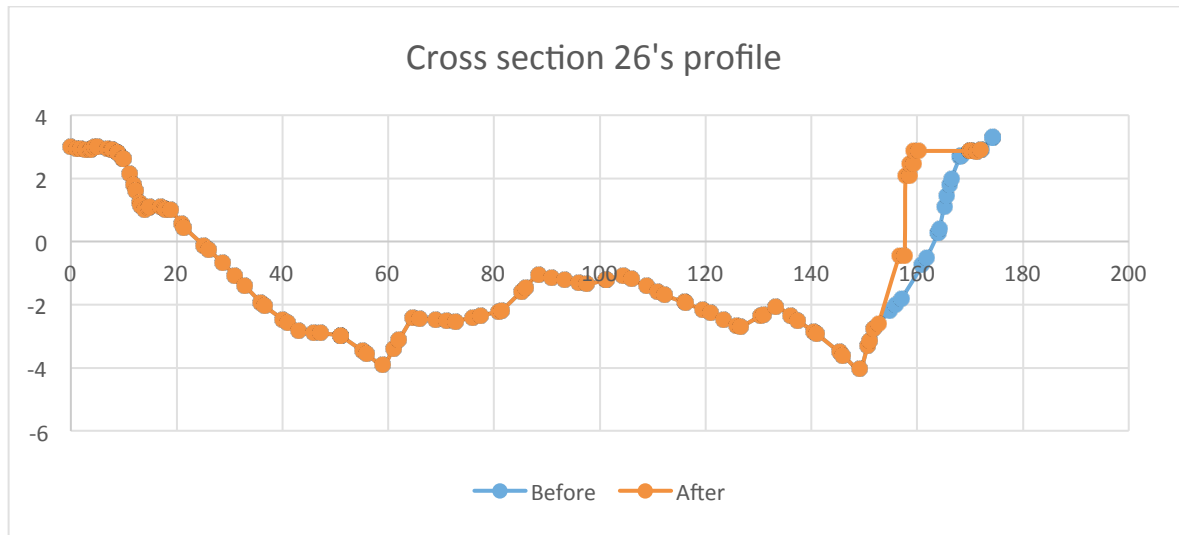


Figure 5: Geometry profiles for Filling work

Two scenarios were used to estimate flow changes after new geometry profile: daily hydropower peaking with low/medium tide water level and flood with return period of 500 years. Both scenarios were tested with low and average tide water level. Low tide is used to estimate maximum water velocity at the interested area, and from that the potential erosion at the river bed. Similarly, average tide water level is used for estimating flood level and to simulate normal river conditions. The downstream and upstream boundary condition setups are described as table below¹:

| Scenario no. | Describe | Upstream boundary condition | Downstream boundary condition |
|--------------|--|--|---|
| 1 | Hydropeaking with low/average tide water level | Normal depth Slope= 0.001, Q = 140m ³ /s | Known water stage 0.73m (low tide) and 1.65m (average tide) |
| 2 | Flood with repeat interval 500 years, low/average tide water level | Normal depth Slope= 0.001, Q ₅₀₀ = 955m ³ /s | |

Table 1: Simulation scenarios

III. RESULTS & DISCUSSIONS

3.1. Calibration results

Calibration results between observed and simulated flow data are displayed as figure below. The X-axis is river length [m] and Y-axis is water elevation [m].

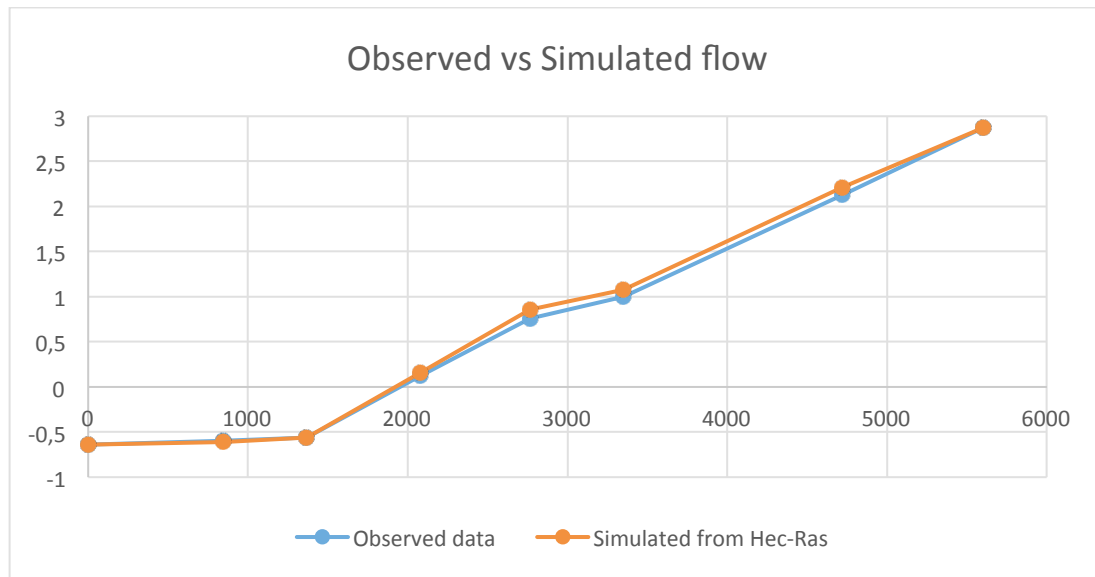


Figure 6: Hec-Ras calibration result

Maximum deviation between observed and simulated water surface elevation are 9.6 cm and 0.1 cm respectively, Nash-Sutcliffe Efficiency value $R^2 = 0.999$. This indicates that the model is able to simulate the flow conditions at this stretch in Nidelva and can be used for further analysis of profile changes.

¹ The data was taken from (Karverket, 2018), (Bævre, 6/2001) and (Tor Haakon Bakken, 2016)

3.2. Effect of modification work on river velocity

Average velocity channel changes under average tide water level

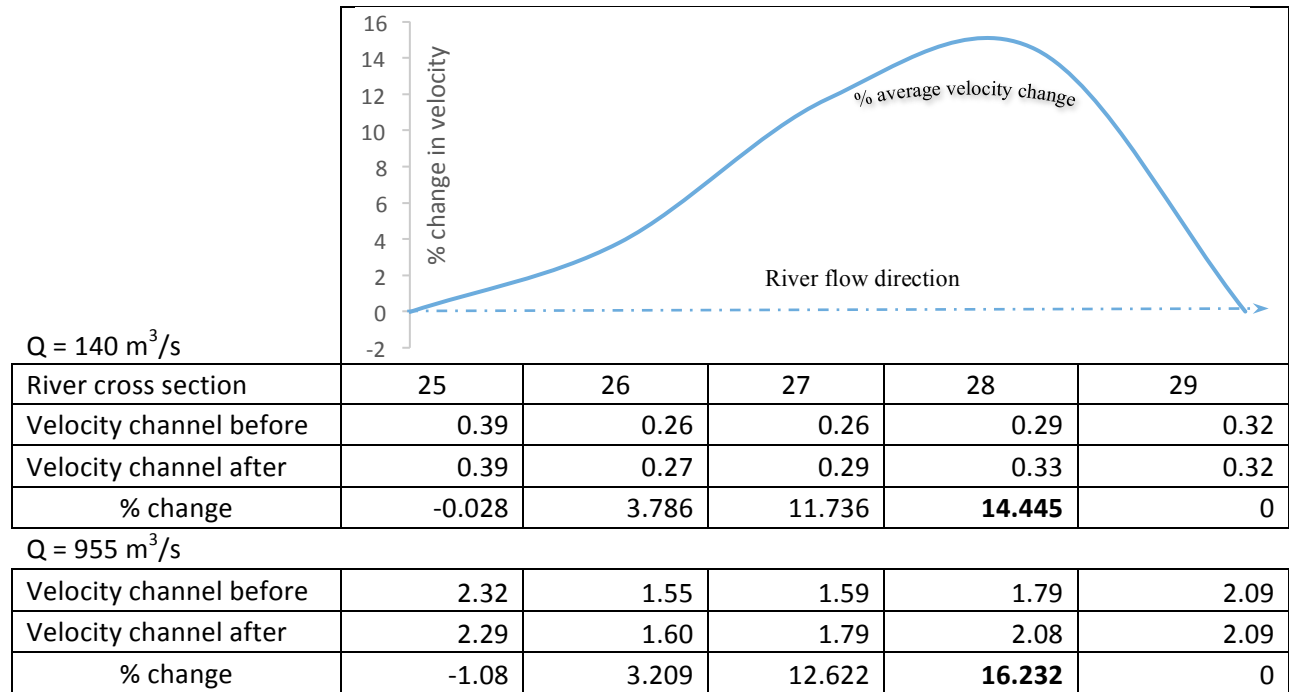


Table 2: Velocity changes under normal tide water surface elevation

Average velocity channel changes under low tide water level

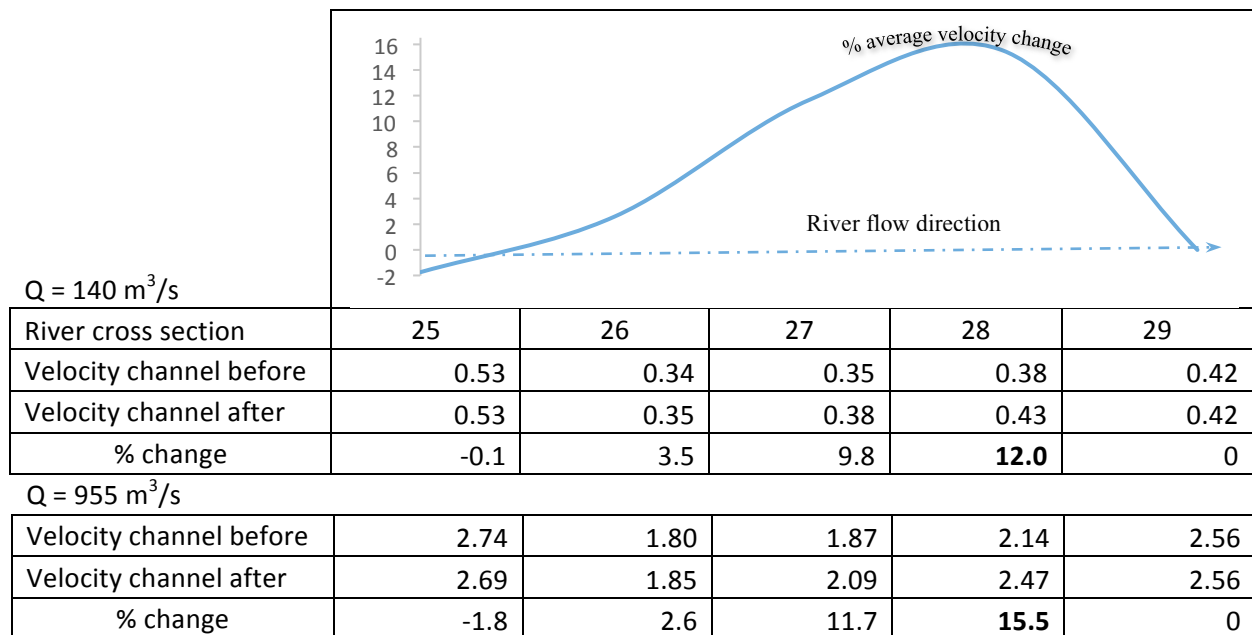


Table 3: Velocity changes under low tide water surface elevation

Following table above, the water velocity is slowed down a little bit at cross section 25 (before the modification work), increase gradually until cross section 28 (at the end of the filling) and return back to normal stage at nearest downstream cross section. Having up to 16% in velocity change indicates that there may be erosion problem at

the river bed, and so this need to be investigated further to identify potential erosion area and propose mitigation work.

Velocity distribution over cross section after modification work

The purpose of velocity distribution mapping is to identify the possible erosion area in the river and to visualize how the velocity changes along the filling area. A total of 45 subsections were divided in each cross section: 5 subsections for each overbank and 35 for main channel.

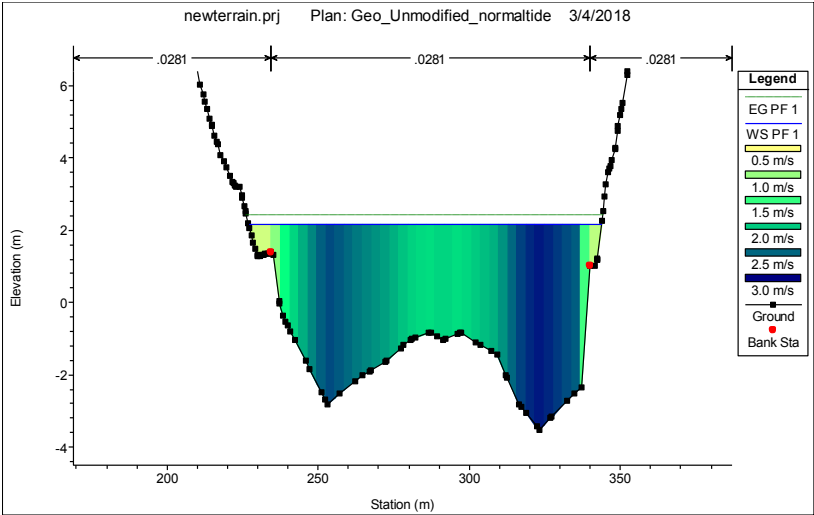


Figure 7: Example of Cross-sectional velocity distribution

After that, the velocity distribution was compared as illustrated in

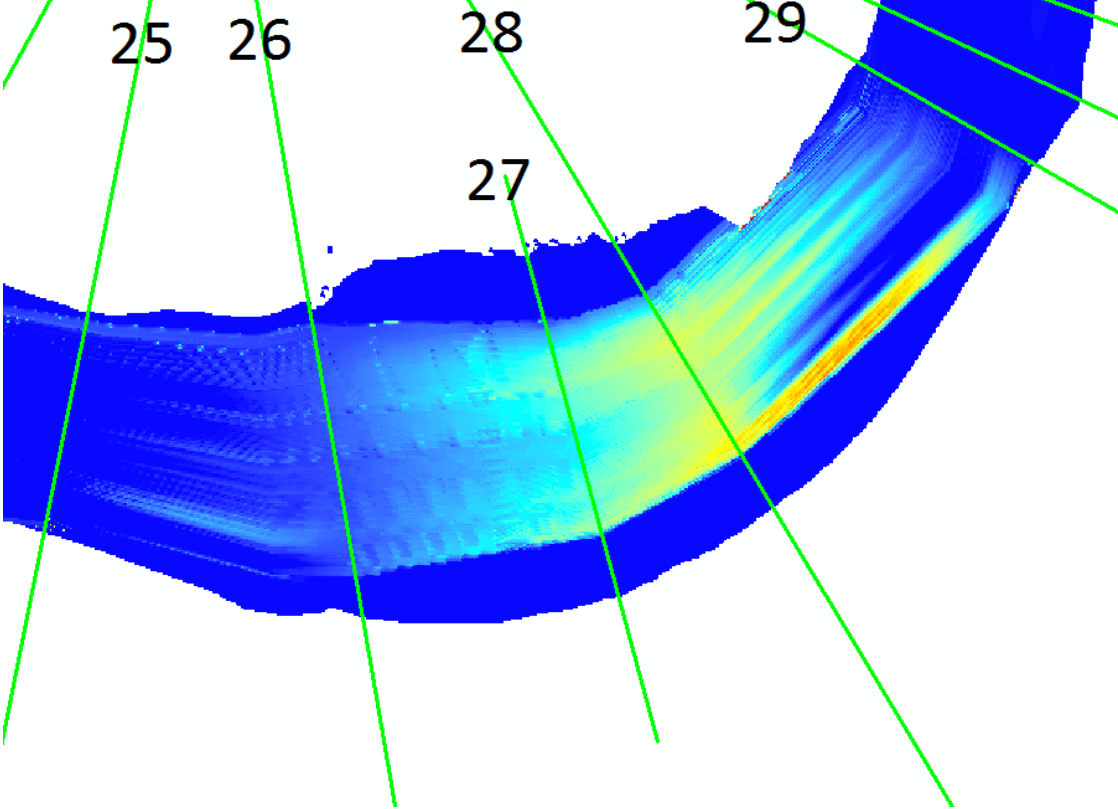


Figure 8. The largest changes are at profile 27 and 28 and are given in table 4 below:

| Scenario | Tide level | Profile 27 | | Profile 28 | |
|-------------------------------------|------------|------------|-------|------------|-------|
| | | Before | After | Before | After |
| Scenario 1; q=140m ³ /s | Low | 0.44 | 0.47 | 0.49 | 0.53 |
| Scenario 1; q=140m ³ /s | Average | 0.32 | 0.35 | 0.36 | 0.4 |
| Scenario 2; q=955 m ³ /s | Low | 2.22 | 2.52 | 2.65 | 2.98 |
| Scenario 2; q=955 m ³ /s | Average | 1.91 | 2.11 | 2.17 | 2.46 |

Table 4: Maximum increase in velocities in the two scenarios and at different tide water level.

where the max velocities increased from 0.44 → 0.47 and 0.49 → 0.53 at profile 27 and 28 respectively at low tide in scenario 1. Similarly, at low tide scenario 2, the velocity increase from 2.22 → 2.52 and from 2.65 → 2.98. Details velocity table is given in appendix 2. Generally, water velocity in average tide condition is lower than in low tide condition for both scenarios.

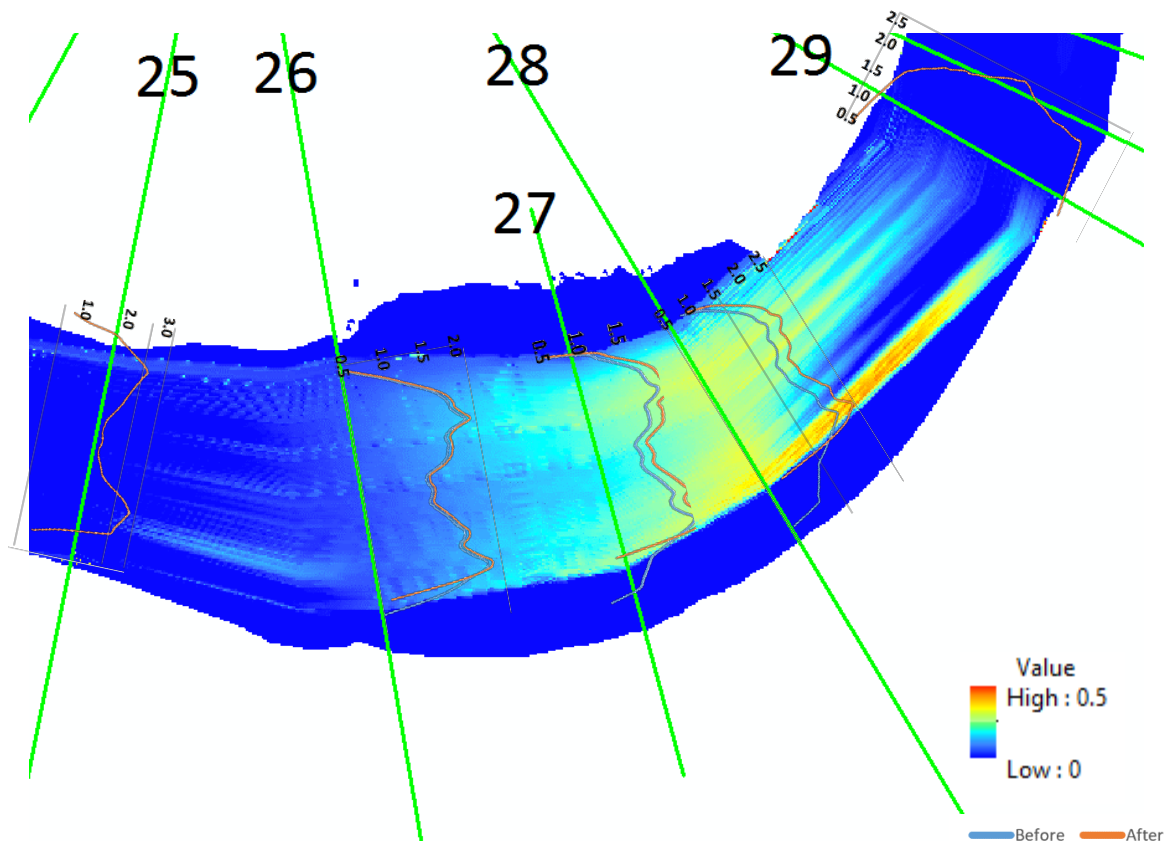


Figure 8: Velocity (lines) before and after filling and change in velocity (map) due to the filling.

3.3. River bed protection proposal

This report uses Shield Diagram (Ponce, 1989) to calculate required mean diameter for shield layer in the river bed using following equations:

$$\tau_{c*} = \tau_{b*} = \frac{\tau_b}{(\rho_s - \rho_f)gD} \#(1)$$

$$\tau_b = \rho_f g h S \#(2)$$

In which:

| | |
|-------------|--|
| τ_{b*} | dimensionless shear stress (Shields parameter) |
| τ_{c*} | dimensionless critical shear stress |
| τ_b | river bed shear stress [N/m ²] |
| D | mean particle diameter [m] |
| ρ_s | density of particle [kg/m ³] |
| ρ_f | density of water [kg/m ³] |
| g | gravity acceleration [m/s ²] |
| h | water depth [m] (includes water stage and min channel elevation) |

For safety reason, min channel elevation and average river slope $S = 0.001$ were used for calculation instead of local slope $S = 0.00073$ (from cross section 25-28).

The calculation used scenario 1, $Q = 140\text{m}^3/\text{s}$ under normal tide condition. The parameters are displayed as table 5:

| Cross section | 27 | 28 |
|---|-----------------------------|-----------|
| Water stage elevation [m] | 1.66 | 1.66 |
| Min channel elevation [m] | -4.0 | -3.97 |
| Dimensionless critical shear stress | 0.06 | 0.06 |
| Density of particles [kg/m ³] | 2650 | 2650 |
| Bottom slope | Use river slope $S = 0.001$ | |
| Bed shear stress calculated from equation (2) [N/m ²] | 56.6 | 56.3 |
| Calculated d_{50} [mm] | 57 | 57 |

Table 5: Proposed shield layer for river bed protection

Priliminary estimates indicates a layer of stone with mean diameter of at least 57 mm is recommended for river bed protection under considered conditions. However, the final decision should be made after performing a field investigation to determine nature grain size distribution at the area and compare with recommended d_{50} .



Figure 9: Area of highest changes in velocity and of potential interest for investigations related to erosion potential

3.4. Floodplain mapping for Q500 after geometry modification

Not any significant change was recognized in floodplain mapping and water level after the modification work compare with NVE's report (Bævre, 6/2001) (right side of figure 10) for the flood with return period 500 years. This means that the filling work have minor effect on flood level downstream and upstream Elgeseter Bru.

| Cross section | Water elevation before [m] | Water elevation after [m] | Increased water level [cm] |
|---------------|----------------------------|---------------------------|----------------------------|
| 25 | 2.15 | 2.19 | 4.1 |
| 26 | 2.18 | 2.21 | 2.9 |
| 27 | 2.12 | 2.11 | -0.8 |

Table 6: Changes in water surface elevation

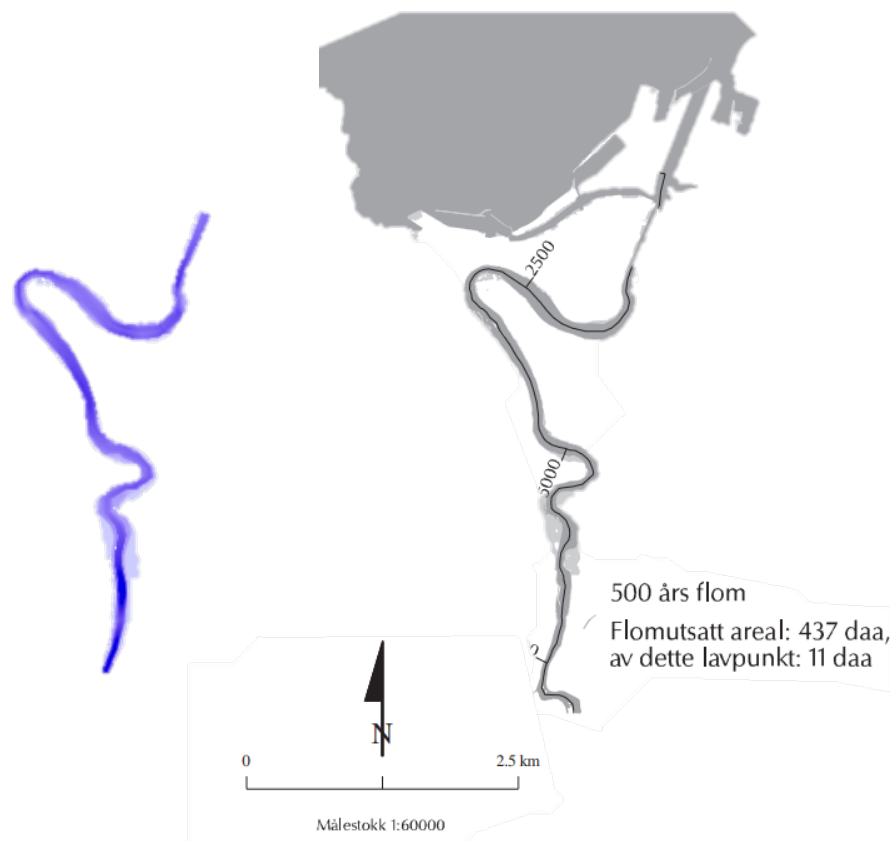


Figure 10: Floodplain mapping result

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- Bævre, I. (6/2001). *Flomsonekart - Delprosjekt Trondheim*. NVE - Norges vassdrags- og energidirektorat.
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- Karverket. (2018). *Tide Tables for the Norwegian Coast and Svalbard*. Kartverket - The Norwegian Mapping Authority.
- Ponce, V. M. (1989). *Engineering Hydrology: Principles and Practices*, page 549 - 552. Prentice Hall.
- Tor Haakon Bakken, T. K. (2016). Simulation of river water temperatures during various hydro-peaking regimes. *Journal of Applied Water Engineering and Research*.

APPENDIX 1

Manning's number table

| | River Station | Frctn (n/K) | n #1 | n #2 | n #3 |
|----|---------------|-------------|----------|----------|----------|
| 1 | 7780.727 | n | 0.037 | 0.037 | 0.037 |
| 2 | 7527.504 | n | 0.037 | 0.037 | 0.037 |
| 3 | 7282.508 | n | 0.037 | 0.037 | 0.037 |
| 4 | 7003.064 | n | 0.0303 | 0.0303 | 0.0303 |
| 5 | 6735.69 | n | 0.0315 | 0.0315 | 0.0315 |
| 6 | 6235.858 | n | 0.0303 | 0.0303 | 0.0303 |
| 7 | 6006.047 | n | 0.0303 | 0.0303 | 0.0303 |
| 8 | 5837.81 | n | 0.0303 | 0.0303 | 0.0303 |
| 9 | 5603.116 | n | 0.0238 | 0.0238 | 0.0238 |
| 10 | 5361.917 | n | 0.0238 | 0.0238 | 0.0238 |
| 11 | 5150.524 | n | 0.0238 | 0.0238 | 0.0238 |
| 12 | 4916.598 | n | 0.0257 | 0.0257 | 0.0257 |
| 13 | 4721.334 | n | 0.0588 | 0.0588 | 0.0588 |
| 14 | 4504.879 | n | 0.0246 | 0.0246 | 0.0246 |
| 15 | 3957.328 | n | 0.0246 | 0.0246 | 0.0246 |
| 16 | 3884.048 | n | 0.0246 | 0.0246 | 0.0246 |
| 17 | 3725.373 | n | 0.0246 | 0.0246 | 0.0246 |
| 18 | 3598.078 | n | 0.0246 | 0.0246 | 0.0246 |
| 19 | 3351.142 | n | 0.0314 | 0.0314 | 0.0314 |
| 20 | 3271.093 | n | 0.0314 | 0.0314 | 0.0314 |
| 21 | 3173.824 | n | 0.0324 | 0.0324 | 0.0324 |
| 22 | 2966.22 | n | 0.0324 | 0.0324 | 0.0324 |
| 23 | 2765.339 | n | 0.0281 | 0.0281 | 0.0281 |
| 24 | 2544.777 | n | 0.0281 | 0.0281 | 0.0281 |
| 25 | 2343.476 | n | 0.0281 | 0.0281 | 0.0281 |
| 26 | 2223.258 | n | 0.0281 | 0.0281 | 0.0281 |
| 27 | 2076.534 | n | 0.0332 | 0.0332 | 0.0332 |
| 28 | 1949.921 | n | 0.0332 | 0.0332 | 0.0332 |
| 29 | 1883.047 | n | 0.0286 | 0.0286 | 0.0286 |
| 30 | 1682.236 | n | 0.0286 | 0.0286 | 0.0286 |
| 31 | 1641.35* | n | 0.0286 | 0.0286 | 0.0286 |
| 32 | 1600.47* | n | 0.0286 | 0.0286 | 0.0286 |
| 33 | 1559.582 | n | 0.0286 | 0.0286 | 0.0286 |
| 34 | 1449.102 | n | 0.0286 | 0.0286 | 0.0286 |
| 35 | 1409.818 | n | 0.0222 | 0.0222 | 0.0222 |
| 36 | 1366.38 | n | 0.03267 | 0.03267 | 0.03267 |
| 37 | 1096.673 | n | 0.03267 | 0.03267 | 0.03267 |
| 38 | 842.5486 | n | 0.028908 | 0.028908 | 0.028908 |
| 39 | 706.7225 | n | 0.028908 | 0.028908 | 0.028908 |
| 40 | 1 | n | 0.028908 | 0.028908 | 0.028908 |

APPENDIX 2

Velocity distribution cross section 27, low tide level condition, $Q = 140 \text{ m}^3/\text{s}$

| Q = 140 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 66.89 | 83.61 | 0.11 | | LOB | 66.89 | 83.61 | 0.12 |
| 2 | Chan | 83.61 | 87.7 | 0.16 | | Chan | 83.61 | 87.7 | 0.18 |
| 3 | Chan | 87.7 | 91.79 | 0.22 | | Chan | 87.7 | 91.79 | 0.24 |
| 4 | Chan | 91.79 | 95.89 | 0.28 | | Chan | 91.79 | 95.89 | 0.3 |
| 5 | Chan | 95.89 | 99.98 | 0.33 | | Chan | 95.89 | 99.98 | 0.36 |
| 6 | Chan | 99.98 | 104.07 | 0.37 | | Chan | 99.98 | 104.07 | 0.39 |
| 7 | Chan | 104.07 | 108.16 | 0.38 | | Chan | 104.07 | 108.16 | 0.41 |
| 8 | Chan | 108.16 | 112.25 | 0.39 | | Chan | 108.16 | 112.25 | 0.42 |
| 9 | Chan | 112.25 | 116.35 | 0.42 | | Chan | 112.25 | 116.35 | 0.45 |
| 10 | Chan | 116.35 | 120.44 | 0.4 | | Chan | 116.35 | 120.44 | 0.43 |
| 11 | Chan | 120.44 | 124.53 | 0.36 | | Chan | 120.44 | 124.53 | 0.39 |
| 12 | Chan | 124.53 | 128.62 | 0.37 | | Chan | 124.53 | 128.62 | 0.39 |
| 13 | Chan | 128.62 | 132.71 | 0.36 | | Chan | 128.62 | 132.71 | 0.39 |
| 14 | Chan | 132.71 | 136.81 | 0.35 | | Chan | 132.71 | 136.81 | 0.38 |
| 15 | Chan | 136.81 | 140.9 | 0.32 | | Chan | 136.81 | 140.9 | 0.34 |
| 16 | Chan | 140.9 | 144.99 | 0.28 | | Chan | 140.9 | 144.99 | 0.31 |
| 17 | Chan | 144.99 | 149.08 | 0.29 | | Chan | 144.99 | 149.08 | 0.32 |
| 18 | Chan | 149.08 | 153.17 | 0.3 | | Chan | 149.08 | 153.17 | 0.32 |
| 19 | Chan | 153.17 | 157.27 | 0.29 | | Chan | 153.17 | 157.27 | 0.31 |
| 20 | Chan | 157.27 | 161.36 | 0.31 | | Chan | 157.27 | 161.36 | 0.33 |
| 21 | Chan | 161.36 | 165.45 | 0.33 | | Chan | 161.36 | 165.45 | 0.35 |
| 22 | Chan | 165.45 | 169.54 | 0.35 | | Chan | 165.45 | 169.54 | 0.38 |
| 23 | Chan | 169.54 | 173.63 | 0.37 | | Chan | 169.54 | 173.63 | 0.4 |
| 24 | Chan | 173.63 | 177.73 | 0.39 | | Chan | 173.63 | 177.73 | 0.42 |
| 25 | Chan | 177.73 | 181.82 | 0.37 | | Chan | 177.73 | 181.82 | 0.4 |
| 26 | Chan | 181.82 | 185.91 | 0.38 | | Chan | 181.82 | 185.91 | 0.4 |
| 27 | Chan | 185.91 | 190 | 0.41 | | Chan | 185.91 | 190 | 0.44 |
| 28 | Chan | 190 | 194.09 | 0.44 | | Chan | 190 | 194.09 | 0.47 |
| 29 | Chan | 194.09 | 198.19 | 0.43 | | Chan | 194.09 | 198.19 | 0.46 |
| 30 | Chan | 198.19 | 202.28 | 0.37 | | Chan | 198.19 | 202.28 | 0.35 |
| 31 | Chan | 202.28 | 206.37 | 0.31 | | Chan | 202.28 | 206.37 | 0.16 |
| 32 | Chan | 206.37 | 210.46 | 0.25 | | | | | |
| 33 | Chan | 210.46 | 214.55 | 0.22 | | | | | |
| 34 | Chan | 214.55 | 218.65 | 0.2 | | | | | |
| 35 | Chan | 218.65 | 222.74 | 0.18 | | | | | |
| 36 | Chan | 222.74 | 226.83 | 0.15 | | | | | |
| 37 | ROB | 226.83 | 243.97 | 0.12 | | | | | |

Velocity distribution Cross section 28, low tide level condition, Q = 140 m³/s

| Q = 140 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 195.18 | 243.97 | 0.14 | | LOB | 195.18 | 243.97 | 0.15 |
| 2 | Chan | 243.97 | 247.6 | 0.17 | | Chan | 243.97 | 247.6 | 0.18 |
| 3 | Chan | 247.6 | 251.23 | 0.23 | | Chan | 247.6 | 251.23 | 0.25 |
| 4 | Chan | 251.23 | 254.86 | 0.28 | | Chan | 251.23 | 254.86 | 0.3 |
| 5 | Chan | 254.86 | 258.49 | 0.33 | | Chan | 254.86 | 258.49 | 0.35 |
| 6 | Chan | 258.49 | 262.12 | 0.36 | | Chan | 258.49 | 262.12 | 0.39 |
| 7 | Chan | 262.12 | 265.75 | 0.39 | | Chan | 262.12 | 265.75 | 0.42 |
| 8 | Chan | 265.75 | 269.38 | 0.4 | | Chan | 265.75 | 269.38 | 0.43 |
| 9 | Chan | 269.38 | 273.01 | 0.42 | | Chan | 269.38 | 273.01 | 0.46 |
| 10 | Chan | 273.01 | 276.64 | 0.42 | | Chan | 273.01 | 276.64 | 0.45 |
| 11 | Chan | 276.64 | 280.27 | 0.39 | | Chan | 276.64 | 280.27 | 0.42 |
| 12 | Chan | 280.27 | 283.9 | 0.4 | | Chan | 280.27 | 283.9 | 0.43 |
| 13 | Chan | 283.9 | 287.53 | 0.4 | | Chan | 283.9 | 287.53 | 0.43 |
| 14 | Chan | 287.53 | 291.16 | 0.39 | | Chan | 287.53 | 291.16 | 0.42 |
| 15 | Chan | 291.16 | 294.79 | 0.36 | | Chan | 291.16 | 294.79 | 0.39 |
| 16 | Chan | 294.79 | 298.42 | 0.36 | | Chan | 294.79 | 298.42 | 0.4 |
| 17 | Chan | 298.42 | 302.05 | 0.37 | | Chan | 298.42 | 302.05 | 0.4 |
| 18 | Chan | 302.05 | 305.68 | 0.37 | | Chan | 302.05 | 305.68 | 0.4 |
| 19 | Chan | 305.68 | 309.32 | 0.39 | | Chan | 305.68 | 309.32 | 0.42 |
| 20 | Chan | 309.32 | 312.95 | 0.41 | | Chan | 309.32 | 312.95 | 0.44 |
| 21 | Chan | 312.95 | 316.58 | 0.42 | | Chan | 312.95 | 316.58 | 0.46 |
| 22 | Chan | 316.58 | 320.21 | 0.44 | | Chan | 316.58 | 320.21 | 0.48 |
| 23 | Chan | 320.21 | 323.84 | 0.44 | | Chan | 320.21 | 323.84 | 0.48 |
| 24 | Chan | 323.84 | 327.47 | 0.44 | | Chan | 323.84 | 327.47 | 0.48 |
| 25 | Chan | 327.47 | 331.1 | 0.46 | | Chan | 327.47 | 331.1 | 0.5 |
| 26 | Chan | 331.1 | 334.73 | 0.49 | | Chan | 331.1 | 334.73 | 0.53 |
| 27 | Chan | 334.73 | 338.36 | 0.46 | | Chan | 334.73 | 338.36 | 0.5 |
| 28 | Chan | 338.36 | 341.99 | 0.42 | | Chan | 338.36 | 341.99 | 0.45 |
| 29 | Chan | 341.99 | 345.62 | 0.38 | | Chan | 341.99 | 345.62 | 0.34 |
| 30 | Chan | 345.62 | 349.25 | 0.33 | | Chan | 345.62 | 349.25 | 0.16 |
| 31 | Chan | 349.25 | 352.88 | 0.28 | | | | | |
| 32 | Chan | 352.88 | 356.51 | 0.25 | | | | | |
| 33 | Chan | 356.51 | 360.14 | 0.23 | | | | | |
| 34 | Chan | 360.14 | 363.77 | 0.21 | | | | | |
| 35 | Chan | 363.77 | 367.4 | 0.18 | | | | | |
| 36 | Chan | 367.4 | 371.03 | 0.16 | | | | | |
| 37 | ROB | 371.03 | 410.61 | 0.1 | | | | | |

Velocity distribution Cross section 27, normal tide level condition, Q = 140 m³/s

| Q = 140 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|------------------|--------------|---------------|----------------|
| | Before | | | | | Cross section 28 | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 66.89 | 83.61 | 0.08 | | LOB | 66.89 | 83.61 | 0.08 |
| 2 | Chan | 83.61 | 87.7 | 0.16 | | Chan | 83.61 | 87.7 | 0.18 |
| 3 | Chan | 87.7 | 91.79 | 0.19 | | Chan | 87.7 | 91.79 | 0.21 |
| 4 | Chan | 91.79 | 95.89 | 0.23 | | Chan | 91.79 | 95.89 | 0.25 |
| 5 | Chan | 95.89 | 99.98 | 0.26 | | Chan | 95.89 | 99.98 | 0.28 |
| 6 | Chan | 99.98 | 104.07 | 0.28 | | Chan | 99.98 | 104.07 | 0.3 |
| 7 | Chan | 104.07 | 108.16 | 0.28 | | Chan | 104.07 | 108.16 | 0.31 |
| 8 | Chan | 108.16 | 112.25 | 0.29 | | Chan | 108.16 | 112.25 | 0.32 |
| 9 | Chan | 112.25 | 116.35 | 0.31 | | Chan | 112.25 | 116.35 | 0.34 |
| 10 | Chan | 116.35 | 120.44 | 0.3 | | Chan | 116.35 | 120.44 | 0.33 |
| 11 | Chan | 120.44 | 124.53 | 0.27 | | Chan | 120.44 | 124.53 | 0.3 |
| 12 | Chan | 124.53 | 128.62 | 0.28 | | Chan | 124.53 | 128.62 | 0.3 |
| 13 | Chan | 128.62 | 132.71 | 0.27 | | Chan | 128.62 | 132.71 | 0.3 |
| 14 | Chan | 132.71 | 136.81 | 0.27 | | Chan | 132.71 | 136.81 | 0.29 |
| 15 | Chan | 136.81 | 140.9 | 0.25 | | Chan | 136.81 | 140.9 | 0.27 |
| 16 | Chan | 140.9 | 144.99 | 0.23 | | Chan | 140.9 | 144.99 | 0.25 |
| 17 | Chan | 144.99 | 149.08 | 0.23 | | Chan | 144.99 | 149.08 | 0.26 |
| 18 | Chan | 149.08 | 153.17 | 0.24 | | Chan | 149.08 | 153.17 | 0.26 |
| 19 | Chan | 153.17 | 157.27 | 0.23 | | Chan | 153.17 | 157.27 | 0.25 |
| 20 | Chan | 157.27 | 161.36 | 0.24 | | Chan | 157.27 | 161.36 | 0.26 |
| 21 | Chan | 161.36 | 165.45 | 0.25 | | Chan | 161.36 | 165.45 | 0.28 |
| 22 | Chan | 165.45 | 169.54 | 0.27 | | Chan | 165.45 | 169.54 | 0.29 |
| 23 | Chan | 169.54 | 173.63 | 0.28 | | Chan | 169.54 | 173.63 | 0.31 |
| 24 | Chan | 173.63 | 177.73 | 0.29 | | Chan | 173.63 | 177.73 | 0.32 |
| 25 | Chan | 177.73 | 181.82 | 0.28 | | Chan | 177.73 | 181.82 | 0.3 |
| 26 | Chan | 181.82 | 185.91 | 0.28 | | Chan | 181.82 | 185.91 | 0.31 |
| 27 | Chan | 185.91 | 190 | 0.3 | | Chan | 185.91 | 190 | 0.33 |
| 28 | Chan | 190 | 194.09 | 0.32 | | Chan | 190 | 194.09 | 0.35 |
| 29 | Chan | 194.09 | 198.19 | 0.31 | | Chan | 194.09 | 198.19 | 0.34 |
| 30 | Chan | 198.19 | 202.28 | 0.27 | | Chan | 198.19 | 202.28 | 0.27 |
| 31 | Chan | 202.28 | 206.37 | 0.24 | | Chan | 202.28 | 206.37 | 0.14 |
| 32 | Chan | 206.37 | 210.46 | 0.21 | | | | | |
| 33 | Chan | 210.46 | 214.55 | 0.19 | | | | | |
| 34 | Chan | 214.55 | 218.65 | 0.18 | | | | | |
| 35 | Chan | 218.65 | 222.74 | 0.17 | | | | | |
| 36 | Chan | 222.74 | 226.83 | 0.16 | | | | | |
| 37 | ROB | 226.83 | 243.97 | 0.11 | | | | | |

Velocity distribution Cross section 28, normal tide level condition, Q = 140 m³/s

| Q = 140 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|--------|--------------|---------------|----------------|
| | Before | | | | | Before | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 195.18 | 243.97 | 0.13 | | LOB | 195.18 | 243.97 | 0.15 |
| 2 | Chan | 243.97 | 247.6 | 0.17 | | Chan | 243.97 | 247.6 | 0.19 |
| 3 | Chan | 247.6 | 251.23 | 0.21 | | Chan | 247.6 | 251.23 | 0.23 |
| 4 | Chan | 251.23 | 254.86 | 0.23 | | Chan | 251.23 | 254.86 | 0.26 |
| 5 | Chan | 254.86 | 258.49 | 0.26 | | Chan | 254.86 | 258.49 | 0.29 |
| 6 | Chan | 258.49 | 262.12 | 0.28 | | Chan | 258.49 | 262.12 | 0.31 |
| 7 | Chan | 262.12 | 265.75 | 0.29 | | Chan | 262.12 | 265.75 | 0.33 |
| 8 | Chan | 265.75 | 269.38 | 0.3 | | Chan | 265.75 | 269.38 | 0.34 |
| 9 | Chan | 269.38 | 273.01 | 0.32 | | Chan | 269.38 | 273.01 | 0.35 |
| 10 | Chan | 273.01 | 276.64 | 0.31 | | Chan | 273.01 | 276.64 | 0.35 |
| 11 | Chan | 276.64 | 280.27 | 0.3 | | Chan | 276.64 | 280.27 | 0.33 |
| 12 | Chan | 280.27 | 283.9 | 0.3 | | Chan | 280.27 | 283.9 | 0.34 |
| 13 | Chan | 283.9 | 287.53 | 0.3 | | Chan | 283.9 | 287.53 | 0.34 |
| 14 | Chan | 287.53 | 291.16 | 0.3 | | Chan | 287.53 | 291.16 | 0.33 |
| 15 | Chan | 291.16 | 294.79 | 0.28 | | Chan | 291.16 | 294.79 | 0.31 |
| 16 | Chan | 294.79 | 298.42 | 0.28 | | Chan | 294.79 | 298.42 | 0.31 |
| 17 | Chan | 298.42 | 302.05 | 0.29 | | Chan | 298.42 | 302.05 | 0.32 |
| 18 | Chan | 302.05 | 305.68 | 0.29 | | Chan | 302.05 | 305.68 | 0.32 |
| 19 | Chan | 305.68 | 309.32 | 0.29 | | Chan | 305.68 | 309.32 | 0.33 |
| 20 | Chan | 309.32 | 312.95 | 0.31 | | Chan | 309.32 | 312.95 | 0.34 |
| 21 | Chan | 312.95 | 316.58 | 0.32 | | Chan | 312.95 | 316.58 | 0.35 |
| 22 | Chan | 316.58 | 320.21 | 0.33 | | Chan | 316.58 | 320.21 | 0.37 |
| 23 | Chan | 320.21 | 323.84 | 0.33 | | Chan | 320.21 | 323.84 | 0.36 |
| 24 | Chan | 323.84 | 327.47 | 0.33 | | Chan | 323.84 | 327.47 | 0.36 |
| 25 | Chan | 327.47 | 331.1 | 0.34 | | Chan | 327.47 | 331.1 | 0.38 |
| 26 | Chan | 331.1 | 334.73 | 0.36 | | Chan | 331.1 | 334.73 | 0.4 |
| 27 | Chan | 334.73 | 338.36 | 0.34 | | Chan | 334.73 | 338.36 | 0.38 |
| 28 | Chan | 338.36 | 341.99 | 0.31 | | Chan | 338.36 | 341.99 | 0.35 |
| 29 | Chan | 341.99 | 345.62 | 0.29 | | Chan | 341.99 | 345.62 | 0.27 |
| 30 | Chan | 345.62 | 349.25 | 0.26 | | Chan | 345.62 | 349.25 | 0.13 |
| 31 | Chan | 349.25 | 352.88 | 0.23 | | | | | |
| 32 | Chan | 352.88 | 356.51 | 0.22 | | | | | |
| 33 | Chan | 356.51 | 360.14 | 0.21 | | | | | |
| 34 | Chan | 360.14 | 363.77 | 0.19 | | | | | |
| 35 | Chan | 363.77 | 367.4 | 0.18 | | | | | |
| 36 | Chan | 367.4 | 371.03 | 0.17 | | | | | |
| 37 | ROB | 371.03 | 410.61 | 0.09 | | | | | |

Velocity distribution Cross section 27, low tide level condition, $Q = 955 \text{ m}^3/\text{s}$

| Q = 955 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 66.89 | 83.61 | 0.52 | | LOB | 66.89 | 83.61 | 0.57 |
| 2 | Chan | 83.61 | 87.7 | 1.12 | | Chan | 83.61 | 87.7 | 1.23 |
| 3 | Chan | 87.7 | 91.79 | 1.35 | | Chan | 87.7 | 91.79 | 1.48 |
| 4 | Chan | 91.79 | 95.89 | 1.6 | | Chan | 91.79 | 95.89 | 1.75 |
| 5 | Chan | 95.89 | 99.98 | 1.82 | | Chan | 95.89 | 99.98 | 1.99 |
| 6 | Chan | 99.98 | 104.07 | 1.97 | | Chan | 99.98 | 104.07 | 2.16 |
| 7 | Chan | 104.07 | 108.16 | 2.03 | | Chan | 104.07 | 108.16 | 2.22 |
| 8 | Chan | 108.16 | 112.25 | 2.09 | | Chan | 108.16 | 112.25 | 2.28 |
| 9 | Chan | 112.25 | 116.35 | 2.22 | | Chan | 112.25 | 116.35 | 2.43 |
| 10 | Chan | 116.35 | 120.44 | 2.13 | | Chan | 116.35 | 120.44 | 2.33 |
| 11 | Chan | 120.44 | 124.53 | 1.95 | | Chan | 120.44 | 124.53 | 2.13 |
| 12 | Chan | 124.53 | 128.62 | 1.97 | | Chan | 124.53 | 128.62 | 2.15 |
| 13 | Chan | 128.62 | 132.71 | 1.96 | | Chan | 128.62 | 132.71 | 2.14 |
| 14 | Chan | 132.71 | 136.81 | 1.92 | | Chan | 132.71 | 136.81 | 2.1 |
| 15 | Chan | 136.81 | 140.9 | 1.76 | | Chan | 136.81 | 140.9 | 1.92 |
| 16 | Chan | 140.9 | 144.99 | 1.62 | | Chan | 140.9 | 144.99 | 1.77 |
| 17 | Chan | 144.99 | 149.08 | 1.66 | | Chan | 144.99 | 149.08 | 1.81 |
| 18 | Chan | 149.08 | 153.17 | 1.68 | | Chan | 149.08 | 153.17 | 1.84 |
| 19 | Chan | 153.17 | 157.27 | 1.64 | | Chan | 153.17 | 157.27 | 1.8 |
| 20 | Chan | 157.27 | 161.36 | 1.71 | | Chan | 157.27 | 161.36 | 1.87 |
| 21 | Chan | 161.36 | 165.45 | 1.81 | | Chan | 161.36 | 165.45 | 1.98 |
| 22 | Chan | 165.45 | 169.54 | 1.9 | | Chan | 165.45 | 169.54 | 2.08 |
| 23 | Chan | 169.54 | 173.63 | 2 | | Chan | 169.54 | 173.63 | 2.18 |
| 24 | Chan | 173.63 | 177.73 | 2.07 | | Chan | 173.63 | 177.73 | 2.26 |
| 25 | Chan | 177.73 | 181.82 | 1.98 | | Chan | 177.73 | 181.82 | 2.17 |
| 26 | Chan | 181.82 | 185.91 | 2.01 | | Chan | 181.82 | 185.91 | 2.2 |
| 27 | Chan | 185.91 | 190 | 2.15 | | Chan | 185.91 | 190 | 2.35 |
| 28 | Chan | 190 | 194.09 | 2.3 | | Chan | 190 | 194.09 | 2.52 |
| 29 | Chan | 194.09 | 198.19 | 2.22 | | Chan | 194.09 | 198.19 | 2.43 |
| 30 | Chan | 198.19 | 202.28 | 1.97 | | Chan | 198.19 | 202.28 | 1.95 |
| 31 | Chan | 202.28 | 206.37 | 1.7 | | Chan | 202.28 | 206.37 | 0.99 |
| 32 | Chan | 206.37 | 210.46 | 1.45 | | | | | |
| 33 | Chan | 210.46 | 214.55 | 1.36 | | | | | |
| 34 | Chan | 214.55 | 218.65 | 1.27 | | | | | |
| 35 | Chan | 218.65 | 222.74 | 1.18 | | | | | |
| 36 | Chan | 222.74 | 226.83 | 1.09 | | | | | |
| 37 | ROB | 226.83 | 243.97 | 0.76 | | | | | |

Velocity distribution Cross section 28, low tide level condition, Q = 955 m³/s

| Q = 955 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 195.18 | 243.97 | 0.96 | | LOB | 195.18 | 243.97 | 1.05 |
| 2 | Chan | 243.97 | 247.6 | 1.19 | | Chan | 243.97 | 247.6 | 1.32 |
| 3 | Chan | 247.6 | 251.23 | 1.46 | | Chan | 247.6 | 251.23 | 1.62 |
| 4 | Chan | 251.23 | 254.86 | 1.67 | | Chan | 251.23 | 254.86 | 1.86 |
| 5 | Chan | 254.86 | 258.49 | 1.88 | | Chan | 254.86 | 258.49 | 2.11 |
| 6 | Chan | 258.49 | 262.12 | 2.06 | | Chan | 258.49 | 262.12 | 2.31 |
| 7 | Chan | 262.12 | 265.75 | 2.16 | | Chan | 262.12 | 265.75 | 2.42 |
| 8 | Chan | 265.75 | 269.38 | 2.22 | | Chan | 265.75 | 269.38 | 2.48 |
| 9 | Chan | 269.38 | 273.01 | 2.34 | | Chan | 269.38 | 273.01 | 2.62 |
| 10 | Chan | 273.01 | 276.64 | 2.3 | | Chan | 273.01 | 276.64 | 2.58 |
| 11 | Chan | 276.64 | 280.27 | 2.19 | | Chan | 276.64 | 280.27 | 2.46 |
| 12 | Chan | 280.27 | 283.9 | 2.23 | | Chan | 280.27 | 283.9 | 2.5 |
| 13 | Chan | 283.9 | 287.53 | 2.23 | | Chan | 283.9 | 287.53 | 2.5 |
| 14 | Chan | 287.53 | 291.16 | 2.17 | | Chan | 287.53 | 291.16 | 2.44 |
| 15 | Chan | 291.16 | 294.79 | 2.05 | | Chan | 291.16 | 294.79 | 2.29 |
| 16 | Chan | 294.79 | 298.42 | 2.07 | | Chan | 294.79 | 298.42 | 2.31 |
| 17 | Chan | 298.42 | 302.05 | 2.1 | | Chan | 298.42 | 302.05 | 2.35 |
| 18 | Chan | 302.05 | 305.68 | 2.09 | | Chan | 302.05 | 305.68 | 2.34 |
| 19 | Chan | 305.68 | 309.32 | 2.16 | | Chan | 305.68 | 309.32 | 2.42 |
| 20 | Chan | 309.32 | 312.95 | 2.26 | | Chan | 309.32 | 312.95 | 2.53 |
| 21 | Chan | 312.95 | 316.58 | 2.34 | | Chan | 312.95 | 316.58 | 2.63 |
| 22 | Chan | 316.58 | 320.21 | 2.43 | | Chan | 316.58 | 320.21 | 2.73 |
| 23 | Chan | 320.21 | 323.84 | 2.41 | | Chan | 320.21 | 323.84 | 2.71 |
| 24 | Chan | 323.84 | 327.47 | 2.41 | | Chan | 323.84 | 327.47 | 2.71 |
| 25 | Chan | 327.47 | 331.1 | 2.52 | | Chan | 327.47 | 331.1 | 2.84 |
| 26 | Chan | 331.1 | 334.73 | 2.65 | | Chan | 331.1 | 334.73 | 2.98 |
| 27 | Chan | 334.73 | 338.36 | 2.51 | | Chan | 334.73 | 338.36 | 2.82 |
| 28 | Chan | 338.36 | 341.99 | 2.32 | | Chan | 338.36 | 341.99 | 2.6 |
| 29 | Chan | 341.99 | 345.62 | 2.13 | | Chan | 341.99 | 345.62 | 2 |
| 30 | Chan | 345.62 | 349.25 | 1.92 | | Chan | 345.62 | 349.25 | 0.96 |
| 31 | Chan | 349.25 | 352.88 | 1.68 | | Chan | | | |
| 32 | Chan | 352.88 | 356.51 | 1.56 | | Chan | | | |
| 33 | Chan | 356.51 | 360.14 | 1.46 | | Chan | | | |
| 34 | Chan | 360.14 | 363.77 | 1.36 | | Chan | | | |
| 35 | Chan | 363.77 | 367.4 | 1.25 | | Chan | | | |
| 36 | Chan | 367.4 | 371.03 | 1.14 | | Chan | | | |

| | | | | | | | | | |
|----|-----|--------|--------|------|--|-----|--|--|--|
| 37 | ROB | 371.03 | 410.61 | 0.65 | | ROB | | | |
|----|-----|--------|--------|------|--|-----|--|--|--|

Velocity distribution Cross section 27, normal tide level condition, Q = 955 m³/s

| Q = 955 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 66.89 | 83.61 | 0.53 | | LOB | 66.89 | 83.61 | 0.59 |
| 2 | Chan | 83.61 | 87.7 | 1.06 | | Chan | 83.61 | 87.7 | 1.17 |
| 3 | Chan | 87.7 | 91.79 | 1.22 | | Chan | 87.7 | 91.79 | 1.35 |
| 4 | Chan | 91.79 | 95.89 | 1.39 | | Chan | 91.79 | 95.89 | 1.54 |
| 5 | Chan | 95.89 | 99.98 | 1.55 | | Chan | 95.89 | 99.98 | 1.72 |
| 6 | Chan | 99.98 | 104.07 | 1.67 | | Chan | 99.98 | 104.07 | 1.84 |
| 7 | Chan | 104.07 | 108.16 | 1.71 | | Chan | 104.07 | 108.16 | 1.89 |
| 8 | Chan | 108.16 | 112.25 | 1.75 | | Chan | 108.16 | 112.25 | 1.93 |
| 9 | Chan | 112.25 | 116.35 | 1.85 | | Chan | 112.25 | 116.35 | 2.04 |
| 10 | Chan | 116.35 | 120.44 | 1.78 | | Chan | 116.35 | 120.44 | 1.97 |
| 11 | Chan | 120.44 | 124.53 | 1.65 | | Chan | 120.44 | 124.53 | 1.82 |
| 12 | Chan | 124.53 | 128.62 | 1.66 | | Chan | 124.53 | 128.62 | 1.84 |
| 13 | Chan | 128.62 | 132.71 | 1.66 | | Chan | 128.62 | 132.71 | 1.83 |
| 14 | Chan | 132.71 | 136.81 | 1.63 | | Chan | 132.71 | 136.81 | 1.8 |
| 15 | Chan | 136.81 | 140.9 | 1.51 | | Chan | 136.81 | 140.9 | 1.67 |
| 16 | Chan | 140.9 | 144.99 | 1.41 | | Chan | 140.9 | 144.99 | 1.56 |
| 17 | Chan | 144.99 | 149.08 | 1.44 | | Chan | 144.99 | 149.08 | 1.59 |
| 18 | Chan | 149.08 | 153.17 | 1.46 | | Chan | 149.08 | 153.17 | 1.61 |
| 19 | Chan | 153.17 | 157.27 | 1.43 | | Chan | 153.17 | 157.27 | 1.58 |
| 20 | Chan | 157.27 | 161.36 | 1.47 | | Chan | 157.27 | 161.36 | 1.63 |
| 21 | Chan | 161.36 | 165.45 | 1.55 | | Chan | 161.36 | 165.45 | 1.71 |
| 22 | Chan | 165.45 | 169.54 | 1.62 | | Chan | 165.45 | 169.54 | 1.79 |
| 23 | Chan | 169.54 | 173.63 | 1.68 | | Chan | 169.54 | 173.63 | 1.86 |
| 24 | Chan | 173.63 | 177.73 | 1.73 | | Chan | 173.63 | 177.73 | 1.92 |
| 25 | Chan | 177.73 | 181.82 | 1.67 | | Chan | 177.73 | 181.82 | 1.85 |
| 26 | Chan | 181.82 | 185.91 | 1.69 | | Chan | 181.82 | 185.91 | 1.87 |
| 27 | Chan | 185.91 | 190 | 1.79 | | Chan | 185.91 | 190 | 1.98 |
| 28 | Chan | 190 | 194.09 | 1.91 | | Chan | 190 | 194.09 | 2.11 |
| 29 | Chan | 194.09 | 198.19 | 1.84 | | Chan | 194.09 | 198.19 | 2.04 |
| 30 | Chan | 198.19 | 202.28 | 1.66 | | Chan | 198.19 | 202.28 | 1.68 |
| 31 | Chan | 202.28 | 206.37 | 1.47 | | Chan | 202.28 | 206.37 | 0.86 |
| 32 | Chan | 206.37 | 210.46 | 1.29 | | | | | |
| 33 | Chan | 210.46 | 214.55 | 1.22 | | | | | |
| 34 | Chan | 214.55 | 218.65 | 1.16 | | | | | |
| 35 | Chan | 218.65 | 222.74 | 1.1 | | | | | |

| | | | | | | | | |
|----|------|--------|--------|------|--|--|--|--|
| 36 | Chan | 222.74 | 226.83 | 1.03 | | | | |
| 37 | ROB | 226.83 | 243.97 | 0.67 | | | | |

Velocity distribution Cross section 28, normal tide level condition, Q = 955 m³/s

| Q = 955 m ³ /s | | | | | | | | | |
|---------------------------|--------|--------------|---------------|----------------|--|-------|--------------|---------------|----------------|
| | Before | | | | | After | | | |
| | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) | | Pos | Left Sta (m) | Right Sta (m) | Velocity (m/s) |
| 1 | LOB | 195.18 | 243.97 | 0.82 | | LOB | 195.18 | 243.97 | 0.92 |
| 2 | Chan | 243.97 | 247.6 | 1.14 | | Chan | 243.97 | 247.6 | 1.28 |
| 3 | Chan | 247.6 | 251.23 | 1.32 | | Chan | 247.6 | 251.23 | 1.49 |
| 4 | Chan | 251.23 | 254.86 | 1.47 | | Chan | 251.23 | 254.86 | 1.66 |
| 5 | Chan | 254.86 | 258.49 | 1.62 | | Chan | 254.86 | 258.49 | 1.83 |
| 6 | Chan | 258.49 | 262.12 | 1.74 | | Chan | 258.49 | 262.12 | 1.97 |
| 7 | Chan | 262.12 | 265.75 | 1.82 | | Chan | 262.12 | 265.75 | 2.06 |
| 8 | Chan | 265.75 | 269.38 | 1.86 | | Chan | 265.75 | 269.38 | 2.1 |
| 9 | Chan | 269.38 | 273.01 | 1.94 | | Chan | 269.38 | 273.01 | 2.2 |
| 10 | Chan | 273.01 | 276.64 | 1.91 | | Chan | 273.01 | 276.64 | 2.17 |
| 11 | Chan | 276.64 | 280.27 | 1.84 | | Chan | 276.64 | 280.27 | 2.08 |
| 12 | Chan | 280.27 | 283.9 | 1.87 | | Chan | 280.27 | 283.9 | 2.11 |
| 13 | Chan | 283.9 | 287.53 | 1.87 | | Chan | 283.9 | 287.53 | 2.11 |
| 14 | Chan | 287.53 | 291.16 | 1.82 | | Chan | 287.53 | 291.16 | 2.07 |
| 15 | Chan | 291.16 | 294.79 | 1.73 | | Chan | 291.16 | 294.79 | 1.96 |
| 16 | Chan | 294.79 | 298.42 | 1.75 | | Chan | 294.79 | 298.42 | 1.98 |
| 17 | Chan | 298.42 | 302.05 | 1.77 | | Chan | 298.42 | 302.05 | 2.01 |
| 18 | Chan | 302.05 | 305.68 | 1.77 | | Chan | 302.05 | 305.68 | 2 |
| 19 | Chan | 305.68 | 309.32 | 1.82 | | Chan | 305.68 | 309.32 | 2.06 |
| 20 | Chan | 309.32 | 312.95 | 1.88 | | Chan | 309.32 | 312.95 | 2.14 |
| 21 | Chan | 312.95 | 316.58 | 1.95 | | Chan | 312.95 | 316.58 | 2.2 |
| 22 | Chan | 316.58 | 320.21 | 2.01 | | Chan | 316.58 | 320.21 | 2.28 |
| 23 | Chan | 320.21 | 323.84 | 2 | | Chan | 320.21 | 323.84 | 2.26 |
| 24 | Chan | 323.84 | 327.47 | 2 | | Chan | 323.84 | 327.47 | 2.26 |
| 25 | Chan | 327.47 | 331.1 | 2.08 | | Chan | 327.47 | 331.1 | 2.36 |
| 26 | Chan | 331.1 | 334.73 | 2.17 | | Chan | 331.1 | 334.73 | 2.46 |
| 27 | Chan | 334.73 | 338.36 | 2.06 | | Chan | 334.73 | 338.36 | 2.34 |
| 28 | Chan | 338.36 | 341.99 | 1.93 | | Chan | 338.36 | 341.99 | 2.18 |
| 29 | Chan | 341.99 | 345.62 | 1.79 | | Chan | 341.99 | 345.62 | 1.73 |
| 30 | Chan | 345.62 | 349.25 | 1.64 | | Chan | 345.62 | 349.25 | 0.81 |
| 31 | Chan | 349.25 | 352.88 | 1.47 | | | | | |
| 32 | Chan | 352.88 | 356.51 | 1.4 | | | | | |
| 33 | Chan | 356.51 | 360.14 | 1.33 | | | | | |
| 34 | Chan | 360.14 | 363.77 | 1.26 | | | | | |

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|----|------|--------|--------|------|--|--|--|--|
| 35 | Chan | 363.77 | 367.4 | 1.18 | | | | |
| 36 | Chan | 367.4 | 371.03 | 1.11 | | | | |
| 37 | ROB | 371.03 | 410.61 | 0.57 | | | | |